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Atomic Layer Deposition – A Novel Method for the Ultrathin Coating of Minitablets

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ABSTRACT

We introduce atomic layer deposition (ALD) as a novel method for the ultrathin coating (nanolayering) of minitables. The effects of ALD coating on the tablet characteristics and taste masking were investigated and compared with the established coating method. Minitables containing bitter tasting denatonium benzoate were coated by ALD using three different TiO₂ nanolayer thicknesses (number of deposition cycles). The established coating of minitables was performed in a laboratory-scale fluidized-bed apparatus using four concentration levels of aqueous Eudragit® E coating polymer. The coated minitables were studied with respect to the surface morphology, taste masking capacity, *in vitro* disintegration and dissolution, mechanical properties, and uniformity of content. The ALD thin coating resulted in minimal increase in the dimensions and weight of minitables in comparison to original tablet cores. Surprisingly, ALD coating with TiO₂ nanolayers decreased the mechanical strength, and accelerated the *in vitro* disintegration of minitables. Unlike previous studies, the studied levels of TiO₂ nanolayers on tablets were also inadequate for effective taste masking. In summary, ALD permits a simple and rapid method for the ultrathin coating (nanolayering) of minitables, and provides nanoscale-range TiO₂ coatings on porous minitables. More research, however, is needed to clarify its potential in tablet taste masking applications.

KEYWORDS

Atomic layer deposition, thin film coating, TiO₂, minitab, taste masking, polymer film coating

ABBREVIATIONS

ALD Atomic layer deposition

40 MCC Microcrystalline cellulose

41 HPC Hydroxypropyl cellulose

42 SPB Sodium phosphate buffer

43 ACN Acetonitrile

44 HPLC High performance liquid chromatography

45 RT Room temperature

46 RH Relative humidity

47 RSD Relative standard deviation

48 SEM Scanning electron microscope

49 SEM-EDS Scanning electron microscope with energy dispersive spectroscopy

50 **1. INTRODUCTION**

51 For tablets, polymer film coating is still the most widely used and efficient taste masking
52 technique in the pharmaceutical industry (Ayenew et al., 2009; Joshi and Petereit, 2013; Sohi et
53 al., 2004). In addition to taste masking purposes, polymer film coating of tablets offers a variety
54 of practical advantages that contribute to their therapeutic effect, as well as ensure patient
55 compliance and tablet product stability throughout their shelf life (Bruce et al., 2011; Felton,
56 2007; Joshi and Petereit, 2013; Pearnchob et al., 2003; Siepmann et al., 2013). With polymer
57 film coating, however, sufficient taste masking and drug release control demand relatively thick
58 polymer films, and consequently, the application of large amounts of polymers (Joshi and

Petereit, 2013). The conventional film coating methods are associated also with laborious, expensive and technical expertise demanding material selection and process development, a lot is required also from coated tablet core and coating formulation design (Joshi and Petereit, 2013). Thus, the pharmaceutical industry is continually searching for new effective and inexpensive coating approaches for tablet taste masking and palatability improvement.

Atomic layer deposition (ALD) is a surface controlled, self-limiting layer-by-layer proceeding coating method for depositing ultra-thin, high quality and conformal thin films, these even on high aspect ratio structures (George, 2010). ALD is commonly used in microelectronics and nanotechnology applications, in functions, where miniaturization of structures requires the control of film thickness at atomic level (George, 2010; Puurunen, 2005). Consequently, the important features of ALD regard surface protection, modification, and functionalization, these in a number of applications benefiting from the characteristics of ALD (George, 2010). In pharmaceuticals, the moisture protective element of ALD coating has been already utilized for nano- and micro-sized drug particles (Carlsson et al., 2016). The ALD technique has been successfully applied also in the design of larger-sized, single particles intended for pharmaceutical powder applications (Hopppu et al., 2015). Here, the present situation is more than inspiring, since the thin film technology combined with material science could lead to new pharmaceutical manufacture and formulation options for fabricating the protective coatings on single drug particles. Bringing such approach to life science markets to serve the evolving needs of drug development, formulation engineering and manufacturing processes could hold great promises on homogeneous drug particles, the creation of new and tailor-made solid dosage forms, improvements in handling moisture sensitive and electrically charged single drug particles, and a decrease in the number of excipients and manufacturing process steps. In

addition to pure drug substances and single particles, ALD coatings could be also applicable for larger, more complex shaped, porous and heterogeneous substrates, such as tablets. The approach seems attractive, as ALD coatings are not only continuous, ultra-thin, dense, and smooth, but also most importantly pinhole-free, very conformal to the substrate, and provide good diffusion barriers with low gas and moisture permeability (George, 2010). In addition, the thin ALD coatings can reach and fill the surface of even the deepest and narrowest voids and pores (Ritala and Leskelä, 2002). Therefore, from the pharmaceutical product design and industry point of view, ALD would provide a very exciting technology not only for drug particle design but also as a potential method for tablet coating purposes.

ALD nanoscale films are formed (grown through deposition) utilizing self-limiting chemical reactions between gaseous precursors chemisorbed on a solid substrate surface. For example, when depositing metal oxide films, compounds of zinc, aluminum or titanium can be used as the metal precursors and water as the oxygen precursor. In many cases, the ALD growth starts by chemisorption of the metal precursor molecules on the hydroxyl groups of the surface. Tablets should allow the initiation of the nanolayering process of ALD, as they are commonly composed of multiple organic excipients containing free hydroxyl groups. In tablets, the number of surface hydroxyl groups required for attachment of molecules can even be created with the small amount of surface moisture readily existing on tablet surfaces and pores. Moreover, from a possible tablet coating point of view, the chemical components like zinc, aluminum and titanium oxides applied by ALD are all established pharmaceutical excipients, and thus their compatibility and safety profiles are well known. Also, compared to the conventional polymer film coating, ALD process is very different. The established polymer coating, performed by a fluidized-bed technique, sets high demands for tablet core strength, and consequently, for tablet formulation

design. During polymer coating in a fluidized-bed, tablets are exposed to frequent collisions, high friction, increased moisture and high temperature. Consequently, tablet cores with limited hardness and mechanical strength are eroded and broken down, especially in the beginning of the coating process until the uniform film coating is formed through concomitant moisture evaporation and polymer particle coalescence (Lehmann, 1997; Mehta, 1997). Thin coating by ALD does not involve such limitations. In flow type ALD reactor, tablet cores are stationary, and are coated during separate surface saturation (deposition) cycles involving chemical interactions (**Fig. 1**). In theory, in ALD involving metal oxides, a cycle of surface saturation takes place through two reaction steps performed commonly in vacuum at controlled temperature. During step one (the first half cycle) the metal precursor such as TiCl_4 vapor, pulsed to the coating chamber, is allowed to react with the free hydroxyl groups on the substrate surface. Therefore, in theory, the chemical pulse saturates the surface with Ti containing groups through molecular bonds. During step two (the second half cycle) the molecularly bonded structures on the substrate surface react with the oxygen precursor (water vapor) and form the first nanolayer of TiO_2 . Between these steps, a purge of inert gas (N_2) is applied in order to remove any excess of precursor and the reaction by-products. The thickness of the films can be controlled by repeating the number of reaction cycles to reach the desired coating thickness. Moreover, compared to the established polymer coating, the ALD process can be completely pre-programmed, and it does not involve high labor or coating raw material related costs.

To date, no well-documented or established study to evaluate the feasibility of ALD for thin coating of tablets has been performed. Lehtonen and co-workers (2013) have evaluated ALD on simple and single material layered tablets, but as pharmaceutical solids traditionally are heterogeneous and complex substrates, a need for a more thorough study on the applicability of

ALD on tablets is evident. Moreover, taste and odor masking capacity of ALD has been studied only on fish oil containing soft gel capsules (Lehtonen et al., 2013). Therefore, we are also completely lacking of information on the applicability and capacity of such ALD ultrathin coatings to improve palatability and taste masking associated with tablets.

Here, we therefore introduce our study describing ALD on minitablets composed of multiple excipients and a bitter tasting model drug. We investigated ALD as a novel technique for thin coating of minitablets, and for masking the bitter taste of model substance of denatonium benzoate. Special attention was paid to the effects of the ALD nanolayering process on the minitablet properties and taste masking efficacy. An established bottom-spray fluidized-bed coating (with a Wurster column set-up) was used as a reference coating technique.

2. MATERIALS AND METHODS

2.1 Materials

Granules were prepared using denatonium benzoate (Sigma-Aldrich, China) as a model substance of a bitter tasting active drug ingredient (0.04% m/m). Microcrystalline cellulose (MCC) (Avicel[®] PH-102, FMC Corporation, Ireland) (63% m/m) and calcium hydrogen phosphate dihydrate (Emcompress[®], Albright & Wilson, Australia) (30% m/m) were used as fillers, and hydroxypropyl cellulose (HPC) (Klucel[®] JXF, Aqualon France SA, France) (3% m/m) and crospovidone (Kollidon[®] CL-F, BASF Corporation, Germany) (4% m/m) as a binder and disintegrant, respectively. Sodium stearyl fumarate (Pruv[®], JRS Pharma, Spain) (1% m/m) was added as a lubricant before tableting.

The synthetic copolymer based on butyl methacrylate, (2-dimethylaminoethyl) methacrylate and methyl methacrylate (1:2:1) (Eudragit[®] E PO, Evonik Industries AG, Germany) was used as a

film forming and taste masking polymer in film coating of minitabets. Lutrol[®] F127 (poloxamer 407, BASF, Germany) (10% m/m, on dry polymer) and dibutyl sebacate (Fluka Chemie AG, Germany) (15% m/m, on dry polymer) were used as the dispersing agent and plasticizer, respectively. Magnesium stearate, Ph.Eur. (donated by Orion Pharma, Finland) was used as an antitacking agent (35% m/m, on dry polymer). Distilled water was used as a dispersion medium for film coating.

ALD TiO₂ films were grown from titanium tetrachloride (TiCl₄) (Sigma-Aldrich, USA) and deionized water. TiO₂ was chosen over zinc and aluminium oxides due to its common use as a coloring agent in pharmaceutical coating formulations. The TiO₂ was considered beneficial also for taste masking purpose due to its hydrophobic (water insoluble) nature.

Distilled water was used as a test medium for tablet disintegration *in vitro*. The *in vitro* dissolution tests were performed using sodium phosphate buffer (SPB) pH 7.6 (US Pharmacopoeia) as a testing medium. The SPB was composed of sodium hydroxide (VWR International S.A.S., France), KH₂PO₄ (Riedel-de Haën, Germany) and distilled water. The uniformity of content test of minitabets was also performed with SPB (pH 7.6).

Acetonitrile (ACN) (Sigma-Aldrich Chemie GmbH, Germany) and aqueous 10mM ammonium acetate pH 4.5 (Sigma-Aldrich Chemie GmbH, Germany) were used as eluents for high performance liquid chromatography (HPLC) analyses conducted for the dissolution and uniformity of content tests.

2.2 Design of experiments

Three different number of coating cycles (100, 300 and 500 cycles) resulting different coating thicknesses were used for the ALD thin coating of minitabets. The numbers of cycles were

selected based on the results of preliminary experiments on ALD. For the polymer coating of minitabets, the design of experiments involved four different polymer coating concentrations of 2, 4, 6 and 8 mg/cm². The levels were selected based on the existing knowledge on the minimum coating thickness of Eudragit® E (1-2 mg/cm²) effective enough for taste masking (Evonik, 2009).

2.3 Preparation of granules and minitabets

Wet granulations of powder mixtures (400 g) were performed in a Diosna high-shear granulator (Dierks&Söhne GmbH, Germany) using distilled water as a granulating liquid. The mixing speeds for impeller and chopper were 600 rpm and 1500 rpm, respectively. The water spraying rate of 140 g/min was used. MCC, calcium hydrogen phosphate dihydrate, HPC and crospovidone were first dry mixed for two minutes. Then, the aqueous solution of denatonium benzoate was pipetted onto the surface of mixed dry powder bed, and subsequently distilled water was sprayed while continuously mixing a powder blend. When the total amount of water (0.45 g/g) was added, granulation was stopped without any kneading phase. The total amount of water was empirically determined based on the preliminary granulation experiments.

Wet granules were wet-sieved (Quadro Comil, Quadro Engineering, Canada) and tray-dried at 40°C for 2 hours, and subsequently at room temperature (RT) for overnight. Prior to tablet compression, the dried masses were sieved (Quadro Comil) with a mesh size of 800 µm. Lubricant (sodium stearyl fumarate) was added and mixed with the granules (Turbula, Willy A. Bachofen AG, Switzerland) for 5 minutes. The masses intended for minitabets compression were allowed to equilibrate at RT/60%RH (relative humidity) for at least 12 hours before tableting.

The granulated masses were tableted at RT/50%RH with a rotary tablet press (Ronchi, Officine Meccaniche F.lli Ronchi, Italy) and single tip punches of 3 mm in diameter to receive round and biconvex minitablets with a target weight of 25 mg and denatonium benzoate strength of 10 µg. Tablets were produced in three separate batches. The average upper and lower punch compression forces (and relative standard deviations, RSD) for the batches I-III were as follows: Batch I 1.8 kN (10.3%) / 0.7 kN (27.1%); Batch II 2.0 kN (11.9%) / 1.8 kN (13.8%); and Batch III 1.7 kN (10.6%) / 1.5 kN (11.6%).

2.4 Polymer film coating of minitablets

The aqueous polymer coating dispersions were prepared by adding emulsifier and plasticizer into a small portion of distilled water and mixing with a magnetic stirrer. Next, the film-forming polymer was progressively added into the aforementioned solution and mixed with a magnetic stirrer for 30 minutes. Magnesium stearate was then homogenously suspended in the remaining portion of water for 30 minutes with a high-shear mixer (Ultra-Turrax, IKA, Germany). The magnesium stearate suspension was added to the polymer dispersion, and the mixture was rapidly homogenized with a high-shear mixer. Finally, the coating suspension was passed through a 500-µm sieve. The final coating dispersions were continuously mixed for overnight with a magnetic stirrer prior to film coating process.

Polymer coating of minitablets was performed in a laboratory-scale fluidized-bed apparatus (Aeromatic AG, Switzerland) equipped with bottom spray-installed Wurster set-up. The height of the Wurster column was 7.0 cm. The nozzle was a Schlick 970/7-1 pneumatic external mixing two-fluid nozzle (Düsen-Schlick GmbH, Germany). The coating processor with instrumentation was connected to a PC and operated via InTouch –software (Wonderware, USA). The coating

batch size was 100 g. The atomizing air pressure was 1.1 bar and the inlet air volume (air flow rate) 12.5 l/s. All coatings were performed in an ambient inlet air RH of $22 \pm 0.4\%$ measured with a Vaisala HUMICAP[®] HMT100 humidity and temperature probe (Vaisala Oyj, Finland). Before each coating experiment, the coating chamber (made of glass) was preheated with an inlet air flow rate of 12.5 l/s, inlet air temperature of 40-50°C, and outlet air temperature of approximately 40°C. The main parameters for nozzle diameter, atomizing air pressure, inlet air volume, inlet air temperature and spraying rate describing the actual coating process are given in **Table 1**. The end-point of a spraying phase was determined as the point where the theoretical polymer amount of 2, 4, 6 and 8 mg/cm² was achieved. The end-point of a drying phase was reached when the difference in RH between the inlet and outlet air was constant. Coated minitables were further tray-dried and cured at 40°C for 24 hours.

2.5 ALD coating of minitables

The ALD was performed in a laboratory-scale flow type ALD reactor (Beneq TFS 200, Finland). Uncoated minitables were placed on the bottom of the reactor plate and pretreated in the reactor at 65°C and at the pressure of 2 mbar for 24 hours prior to deposition to remove the moisture from the tablets. The thin nanolayers of TiO₂ were grown on minitables from TiCl₄ and water at 65°C. Nitrogen (N₂) was used as a carrier and purging gas. The TiCl₄ and water were evaporated from the sources at 20°C. The cycle consisted of a 300 ms TiCl₄ pulse, 20 s N₂ purge, 300 ms water pulse and 30 s N₂ purge. The number of ALD cycles was 100, 300 and 500 corresponding to approximately 10, 30 and 50 nm film thicknesses measured from the silicon reference sample processed in the same runs. Using the approximate coating film thickness (10, 30 and 50 nm) and the density of TiO₂ (4.23 g/cm³), the amount of TiO₂ coating was 0.0042 mg/cm², 0.0127 mg/cm² and 0.0212 mg/cm² corresponding to respective ALD cycles of 100, 300 and 500. After

the coating, the minitablets were collected from the coating chamber and were stored in carefully closed glass vials at RT prior to further analyses.

2.6 Characterization of minitablets

The surface morphology of uncoated and coated minitablets containing denatonium benzoate was studied using a scanning electron microscope (SEM) (FEI Quanta FEG250, FEI Inc., USA) at the Electron Microscope Unit, Institute of Biotechnology, Helsinki, Finland. Dry platinum-coated samples were scanned using a voltage of 10 kV. The surface morphology and surface content analysis for uncoated and TiO₂ coated minitablets (500 cycles) were further determined by field emission scanning electron microscope with energy dispersive spectroscopy (SEM-EDS) (Hitachi S-4800 equipped with Oxford INCA 350) at the Department of Chemistry, Helsinki, Finland. The measurements were performed using the voltage of 20 kV. Minitablet samples were coated with carbon prior to the measurements.

The height of minitablets was measured with a Sony digital micrometer (Sony Digital Indicator U30-F, Sony, Japan) (n=10). The uniformity of mass and uniformity of content tests were performed according to Ph. Eur. (the tests described in the chapters 2.9.5 and 2.9.6, respectively).

The dissolution of denatonium benzoate minitablets was determined using a modified Ph.Eur. (2.9.3) basket method and apparatus A (Erweka DT6, Erweka GmbH, Germany) (n=4). The dissolution medium was 40 ml of SPB (pH 7.6) at 37 - 38°C. The basket rotation speed was 50 rpm. The samples were collected manually at time periods of 0 and 15 s, and then, after every 30 seconds until the end-point of 6 minutes 15 s. The dissolution sample size for denatonium benzoate containing minitablets was 250 µl. Prior to HPLC analysis, the samples were

centrifuged (13,200 rpm/5 min) and pipetted into HPLC sampling vials. HPLC analyses were performed within 24 hours after dissolution testing.

The disintegration tests of uncoated and coated minitables were performed using a Sotax DT3 tablet disintegration apparatus (Sotax AG, Switzerland). The method was slightly modified for small minitables from the standard Ph.Eur. tablet disintegration method (2.9.1): the bottom of each testing cylinder was covered with a stainless steel mesh (with an average mesh size 0.2 mm) to prevent a small tablet dropping down to the bottom of a test glass beaker.

The tablet breaking force (tablet hardness) was determined using a Schleuniger-2E tablet hardness tester (Dr. K. Schleuniger & Co., Switzerland) with a slight modification compared to the Ph.Eur. method (2.9.8). Instead of determining the load required to crush a tablet diametrically (when placing tablets diametrically onto their flat side between the jaws), tablets were placed diametrically on their edge (edge) between the jaws. This was due to the occasional non-detectability of the load needed to crush the minitab placed diametrically onto their flat side.

2.7 HPLC assays

For the uniformity of content and dissolution tests, the samples were analyzed using an Agilent 1100 series HPLC system (Agilent Technologies, USA) equipped with an UV-Vis detector. The reverse-phase column Zorbax Eclipse Plus C18 (100x4.6 mm, 3.5 μ m) (Agilent Technologies, USA) was utilized in the analyses.

The flow rate of eluent mixture of ammonium acetate (10 mM, pH 4.5):ACN was 1 ml/min. Denatonium benzoate was detected at wavelength 210 nm at 25°C. For uniformity of content test, the corresponding ratio of the eluents and the retention time of denatonium benzoate was

55:45 and 1.8 min (for the uncoated and the polymer coated minitabets), and 60:40 and 2.4 min (for the uncoated and the TiO₂ coated minitabets). For dissolution testing of uncoated and both polymer and TiO₂ coated minitabets, the ratio of the eluents was 60:40, and the retention time of denatonium benzoate was 2.4 min.

2.8 Statistical method of calculation

The Student's t-test (two-tailed distribution, two-sample unequal variance) was used for the calculation of statistical differences between uncoated and coated tablets, these in the results of tablet dissolution, uniformity of tablet mass and denatonium benzoate content, tablet disintegration rate, breaking force and height. Difference between uncoated and coated tablets was considered statistically significant with $p < 0.05$.

3. RESULTS

3.1 Content and dimensions of minitabets

Table 2 shows the weight, active ingredient content, disintegration time, breaking force and height of uncoated and coated tablets. For TiO₂ coated minitabets, no statistically significant ($p < 0.05$) change in the tablet height between uncoated tablets and different coatings of 100, 300 or 500 cycles was revealed, though the average tablet height of uncoated tablets was slightly higher than that of coated minitabets. As expected, similarly to tablet height, no changes in the weight of TiO₂ coated minitabets or denatonium benzoate content were revealed.

Compared to uncoated tablets, a slight decrease in the denatonium benzoate content was observed in polymer film coated tablets, the difference being statistically significant with polymer amounts of 6 and 8 mg/cm² (Table 2). In comparison to uncoated tablets, film coated

tablets exhibited also an increase in the tablet height and weight, particularly with polymer amounts of 4, 6 and 8 mg/cm² (tablet height) and with polymer amounts of 2, 6 and 8 mg/cm² (tablet weight). The difference between uncoated and polymer coated tablets seemed gradual and in accordance with increased polymer amount. The increase in tablet height with coating of polymer amounts of 2 and 4 mg/cm² was lower than with polymer amounts 6 and 8 mg/cm². The highest increase in tablet height and weight was observed with polymer amount of 8 mg/cm². Tablet height remained relatively unchanged with polymer amount of 2 mg/cm² when compared to uncoated tablets. However, the average weight of minitables with coating of 2 mg/cm² decreased in comparison to uncoated minitables.

3.2 Minitablet hardness

The TiO₂ coating significantly ($p < 0.05$) decreased the breaking force (hardness) of minitables in comparison to uncoated minitables (Table 2). No difference in the breaking force of minitables between different TiO₂ thicknesses (100, 300 and 500 cycles) was revealed.

Surprisingly, the breaking force of polymer film coated tablets was also lower than that of uncoated minitables. No changes in the breaking force were seen between the minitables coated with polymer concentration of 2 and 4 mg/cm², and between the minitables coated with polymer concentration of 6 and 8 mg/cm².

3.3 Disintegration in vitro

The disintegration times of uncoated, TiO₂ coated, and polymer film coated minitables are presented in Table 2. Surprisingly, the disintegration time of TiO₂ coated minitables was clearly shorter ($p < 0.05$) than that obtained with uncoated minitables. No clear differences in the disintegration times between ALD coated tablets (100, 300 and 500 cycles) were revealed as the

disintegration tendency described by the average disintegration time was only slightly decreasing over coating cycles.

Surprisingly, the disintegration time of minitables coated with polymer concentrations of 2 and 4 mg/cm² was shorter in comparison to that of uncoated minitables. However, minitables coated with polymer concentration of 4 mg/cm² disintegrated more slowly than minitables coated with 2 mg/cm² polymer concentration. In addition, the disintegration time of minitables coated with polymer concentration of 6 mg/cm² was shorter than that of minitables coated with higher amount (8mg/cm²) of polymer, but compared with uncoated tablets, the difference with polymer amount of 6 mg/cm² was not statistically significant. As expected, the disintegration of minitables containing polymer concentration of 8 mg/cm² was slower than that of uncoated or other polymer coated tablets of the study. In addition, the minitables coated with higher polymer concentration of 8 mg/cm² exhibited a clear lag-time prior to disintegration which was not observed with the TiO₂ coated minitables.

3.4 Dissolution in vitro

The dissolution profiles of uncoated, ALD coated (TiO₂) and polymer film coated minitables are shown in **Fig. 2**. With both uncoated and ALD coated minitables (100, 300 and 500 cycles), the lag-time for denatonium benzoate release was very short (less than 45 seconds). With polymer film coated minitables, denatonium benzoate release was detected at 45 s (2, 4 and 6 mg/cm²) and at 1 min 15 s (8 mg/cm²).

At 45 seconds, the highest amount of released denatonium benzoate was detected for minitables containing 2 mg/cm² and 4 mg/cm² of coating polymer, while no difference in the released amount of denatonium benzoate was revealed between uncoated and polymer film coated (6

mg/cm²) minitabets. The polymer film coating of minitabets (2, 4 and 6 mg/cm²) increased the release rate of denatonium benzoate compared to that obtained with uncoated minitabets. However, when the highest amount of coating polymer (8 mg/cm²) was used, the minitabets exhibited a clear delay in the release rate of denatonium benzoate.

TiO₂ ALD coating on minitabets had only a small effect on the release rate and profile of denatonium benzoate. The slowest release of denatonium benzoate was revealed for 500 cycles ALD TiO₂ coated minitabets. Application of 100 and 300 cycles in the TiO₂ ALD coating of minitabets exhibited only a slight delay in the release rate of denatonium benzoate compared to that obtained with uncoated minitabets.

3.5 SEM and EDS

The SEM images defining the internal structure and surface morphology of uncoated and coated minitabets are shown in **Fig. 3**. The SEM-EDS linescans of TiO₂ ALD coated minitabets (500 cycles) are presented in **Fig. 4** (intact minitabets) and **Fig. 5** (the cross-section of the minitabets). The surface of uncoated minitabets (Fig. 3A) was relatively smooth with dark and white areas, and application of TiO₂ ALD coating had virtually no effect on the surface morphology of minitabets (100 cycles in Fig. 3B, 300 cycles in Fig. 3C, and 500 cycles in Fig. 3D). The surface of polymer film coated tablets (2 mg/cm² in Fig. 3E) revealed rough eroded holes on an uneven tablet surface. Smoother and more even minitabets surfaces were obtained with higher coating polymer concentrations (4 mg/cm² in Fig. 3F, 6 mg/cm² in Fig. 3G, and 8 mg/cm² in Fig. 3H).

The SEM-EDS linescan of the TiO₂ ALD coated tablet surface revealed the presence of titanium and chlorine on the surface of minitabets (Fig. 4). Moreover, the intensity of the titanium signal seemed to be in accordance with the intensities of elements of calcium and phosphorous (arrows

in Fig. 4 for titanium). With the cut ALD coated minitab, the intensity of the titanium signal was verified to be exceptionally high on the minitab surface but decreased rapidly when moving towards the minitab core (Fig. 5). The penetration of Ti into the structure of the tablet was reaching an approximate depth of 0.2 mm. No titanium was present at the surface of uncoated minitab (data not shown).

4. DISCUSSION

4.1 Effect of coating method on the properties of minitab

It is well known that the tablet cores in a conventional fluidized-bed polymer coating process are exposed to a long-term attrition (friction) and collisions resulting in the erosion (even breakage) of tablets during processing. However, the ALD thin coating of tablets with TiO₂ in flow type ALD reactor is a much more gentle procedure as the tablets are stationary during coating and thus, are not susceptible to kinetical attrition or collisions similar in fluidized-bed. Thus, no statistically significant differences between uncoated and ALD-coated tablets were revealed for tablet integrity, weight, dimensions, or active drug content.

Surprisingly, however, the breaking force (hardness) and disintegration time of minitabs decreased after ALD coating. This was confusing, especially as in the literature, the ALD coated 3-layer tablets have been reported to comply with the specifications for hardness and disintegration time of such dosage forms (Lehtonen et al., 2013). Thus, by contrast to a decrease in the minitab strength and disintegration, a delay was our more likely expectation, particularly as in theory, the chosen minitab formulation was thought to support the formation of even, pinhole-free and moisture protective TiO₂ ALD nanolayers. Moreover, in the present study, the experimental composition of minitab core was considered ideal for ALD thin

390 coating, since the presence of the free hydroxyl groups on the surface of MCC in addition to the
391 tablet surface moisture were expected to provide excellent binding sites for TiCl_4 . This should
392 foster also the formation of homogeneous TiO_2 nanolayers on tablet surfaces, voids and crevices,
393 thus reducing the core ability to interact with its surroundings. Moreover, the low deposition
394 temperature of 65°C used in the present study was not harmful for the tablet core. In the
395 literature, TiO_2 ALD nanolayering of tablets using TiCl_4 -water chemistry has been successfully
396 conducted at temperatures even lower than 65°C (Lehtonen et al., 2013). The decrease in
397 hardness and disintegration time of minitables after ALD thin coating can be explained by the
398 fact that pharmaceutical tablets are heterogeneous and porous solid systems, unlike to the
399 substrates traditionally used in ALD thin coating. Moreover, the real ALD film growth
400 mechanism may not be as simple as the theory outlines.

401 A short interaction between moisture and heterogeneous tablet core components (such as the
402 disintegrant crospovidone or MCC) can cause the microerosion of tablets during an ALD thin
403 coating processing. It is evident that this also induces the creation of new pores, new open intact
404 tablet surfaces, and even new complicated pore networks to the tablet structure. Moreover, the
405 risk for microerosion can increase (especially at low temperatures) because of the liberation of
406 the reaction side product of hydrochloric acid gas, due to TiCl_4 -water chemistry, adsorbing onto
407 the TiO_2 surface (Ritala et al., 1993). As microerosion enlarges, the active surface area of tablets
408 requiring coating also becomes larger. This means that during deposition the exposed new
409 surfaces and pore networks are not likely to be adequately covered by TiO_2 nanolayers, simply
410 due to insufficient amount of coating precursor. Thus, microerosion could reduce the layer
411 moisture protecting capability and accelerate the tablet disintegration rate, as well as decrease the
412 tablet hardness. Moreover, in theory, the TiO_2 is covalently bonded to the hydroxyl-covered

413 substrate surface. This could indicate the formation of a completely new chemical component
414 with characteristics totally different from those of the original substance. Also, the variation in
415 the configuration and the level of the hydroxyl-grouped surfaces may complicate the film growth
416 (Ritala et al., 1993). It is evident that areas with uneven and variable level of hydroxyl groups
417 lead to uneven TiO₂ layers. Furthermore, the amphoteric chemical behavior of TiO₂ surface due
418 to differently orientated and bonded hydroxyl groups on the TiO₂ surface (Parfitt, 1976) can lead
419 to additional reactions other than with TiCl₄. Low deposition temperatures used in the TiO₂ ALD
420 thin coating can also induce the formation of chemical impurities (residual ions), such as
421 chlorine in ALD thin films originating from TiCl₄ precursor ligands (Ritala et al., 1993; Jögi et
422 al., 2006), and may therefore change the film properties. In addition, at this growth temperature
423 ALD TiO₂ thin films are in fact amorphous and may thus have increased intensity for moisture
424 related interactions.

425 The success of TiO₂ ALD coating is therefore very much dependent on the tablet core
426 composition, structure and properties. With the present minitables, phenomena occurring on the
427 heterogeneous tablet surface are hence strongly emphasized. Lehtonen and co-workers (2013)
428 investigated the ALD thin coatings applied to the tablets composed of three-layered
429 pharmaceutical solids containing layers of probiotics and vitamin C. Pharmaceutical tablets are
430 commonly compressed from heterogeneous mixtures. Due to such complex compositions, the
431 coatings applied to the outer surface of tablet cores are exposed to multiple different
432 components, which all have characteristic porosity and interaction capabilities, e.g. with
433 moisture or chemicals. Consequently, the formation of even and pinhole-free TiO₂ ALD
434 nanolayers is greatly affected by the chemical composition of the tablet surface (especially, the
435 excipients rich on hydroxyl groups play a key role), and most likely also by surface moisture. In

other words, the formation and growth of TiO₂ thin films is fostered by the surfaces exhibiting very high hydroxyl group density. In addition, the pore density, size and tortuosity of excipients can play a crucial role affecting TiO₂ ALD thin films. Depending on the physicochemical characteristics, the active outer surface area of tablet excipients can be very different due to interaction with moisture. Consequently, deep voids or complex pore structures can result in inadequate TiO₂ ALD nanolayer formation and growth. Moreover, the formation of intact TiO₂ ALD coating in tablet pores is most likely to be fostered by the presence of high hydroxyl group density. With the present minitables, it is evident that excipients and/or denatonium benzoate interact with titanium to different extent and mechanism, thus affecting the formation of nanolayers. Therefore, the reason for the unexpected decrease in the hardness and disintegration time of coated minitables is most likely the heterogeneity and physicochemical diversity of chemical components in the tablet surface.

ALD thin coating has a number of advantages compared to a traditional fluidized-bed film coating method. The TiO₂ ALD nanolayering is a gentle procedure in a flow type reactor without any actual collision related impact on tablets. On the contrary, the traditional fluidized-bed coating requires adequate mechanical strength of tablet cores, and appropriate and well-designed tablet compositions. In a fluidized-bed coating process, tablet breakage takes place readily due to a long-term collision and abrasion during fluidization, and due to the elevated temperature and humidity conditions during polymer dispersion spraying and drying. Moreover, particles detached from tablet cores can disturb the formation of even polymer coating and lead to a great variation in an active ingredient content, disintegration and dissolution of tablets. It is also well-known that traditional polymer film coating can lead to a significant increase in tablet weights

and delay in disintegration times, especially if thick polymer coatings involving high amounts of polymer are used.

In our study, fluidized-bed polymer film-coated tablets exhibited a clear decrease in hardness (breaking force), tablet weight and denatonium benzoate content compared to the corresponding uncoated tablets, all mostly related to tablet erosion and breakage during film coating process. The possibility for tablet breakage was expected to be avoided with the inclusion of MCC as a main component in the tablet core formulation. MCC deforms plastically under compression and maximizes the area of inter-particle hydrogen bonding, thus increasing tablet mechanical strength and hardness (Bolhuis and Lerk, 1973). Consequently, no friability test was performed for the MCC containing minitablen cores, and also because the tablet friction during the strong fluidization in the actual fluidized-bed apparatus was considered to provide a more accurate result for tablet friability. MCC can also entrap and hold significant amounts of moisture inside its structure (Zografi and Kontny, 1986), thus making it an excipient of choice for the moisture-sensitive ingredients in tablets. Its moisture related interactions during processing and drying are also well-documented (Luukkonen, 2001; Luukkonen et al., 2001; Kleinebudde, 1994).

In fluidized-bed coating, several process-related conditions (e.g. high humidity, agitation and elevated temperatures during spraying and drying) can affect the final polymer film coated tablets. Using aqueous polymer coating dispersions, the process-induced changes (interactions) are naturally more evident if the tablet cores are composed of amorphous and/or moisture sensitive excipients, e.g. binders (HPC) or disintegrants (crospovidone) (Joshi and Petereit, 2013). These changes are also greatly dependent on the duration (time) of a fluidized-bed process. In our study, the most significant process-induced changes were resulted by the decrease of the hardness of minitablen.

481 We found that the minitabket cores used in the fluidized-bed polymer coating experiments did not
482 completely withstand the process conditions (agitation, high humidity and elevated temperature).
483 This was obviously partly due to the interaction of MCC with moisture, thus leading to a notable
484 decrease in the mechanical strength (hardness) of tablets. This finding is also in good agreement
485 with that reported in the literature (Westermarck et al., 1999). Moreover, the moisture-induced
486 softening and erosion of tablet cores are most likely fostered with the presence of moisture-
487 sensitive HPC and crospovidone in the tablet formulation. The deteriorating influence of
488 moisture and agitation continues until the uniform and intact film coating is formed around
489 tablets. Deterioration of polymer film-coated tablets can continue even after a coating process, if
490 moisture is entrapped inside the tablet core and polymer film.

491 To avoid tablet deterioration related problems with moisture-sensitive tablet formulations,
492 spraying of polymer dispersion in fluidized-bed coating could be started with a small amount of
493 dispersion followed by an immediate drying phase. This kind of spraying protocol is expected to
494 enhance the initial film formation, thus protecting tablet cores from future moisture interactions.
495 In the fluidized-bed film coating of minitabkets, it is also important to control and optimize the
496 spraying properties of dispersion such as droplet size in order to avoid over-wetting and
497 subsequent softening of tablet cores. Compared to large-sized tablets, adequate coating of
498 minitabkets containing swellable excipients in particular requires higher amounts of coating
499 polymer due to the larger outer surface area of such minitabkets (Mehta, 1997). This is even more
500 important with taste masking film coatings where the applicability and efficacy of coating is
501 dependent of film thickness and intactness. One option to overcome the challenge associated
502 with the larger outer surface area of minitabkets is to prolong contact time of tablet cores with the

coating polymer dispersion, e.g. by modifying a Wurster column set-up or by increasing a coating process time. However, such changes will impact also the other coating parameters.

4.2 Taste masking efficacy of minitablets

Sensing the taste requires the initial interaction of the tablet with moisture (saliva), and subsequent tablet disintegration and dissolution of tastant in the oral cavity. The sensory information from the tongue is then instantly transmitted via neural pathways to the brain to be interpreted as taste perception (Thombre, 2004). The requirement of saliva solubility makes the taste a chemical sense. Normally, the physiological pH of human saliva is neutral varying from pH 6 to pH 7.5 (Tenovuo, 1995). The diet can greatly affect the pH of saliva. Therefore, the typical pH of saliva in herbivores and omnivores is more alkaline than the saliva pH of carnivores.

For the evaluation of minitablet dissolution and bitter taste masking efficacy *in vitro*, we used an aqueous buffer solution pH 7.6 representing the average pH for the saliva. The expected residence time of tablets in the mouth was also taken into account in a study protocol. In our study, a mouth residence time longer than 45 seconds without detected bitter tasting denatonium benzoate was required for effective minitablet taste masking, as on average, the time period of a solid dosage form to remain in the mouth is relatively short ranging from a few seconds to 30-60 seconds (Joshi and Petereit, 2013). In this study, the modified disintegration and dissolution tests of minitablets *in vitro* were used to indirectly show the taste masking efficacy of the coated tablets. With better mimicking of the soft tissue function and conditions in the mouth and gastrointestinal system, the more gently proceeding tablet dissolution test with results on

detected denatonium benzoate release were emphasized when used as a tool for the rapid taste masking efficacy evaluation purposes of the coated minitables of the study.

The *in vitro* dissolution results of TiO₂ ALD coated minitables were in accordance with the *in vitro* disintegration times of the respective nanolayered minitables (Fig. 2). The early denatonium benzoate release from both uncoated and TiO₂ ALD coated minitables was observed at 45 s. This suggests that the coating thickness of the present ALD nanolayered minitables (i.e., the coating cycles of 100, 300 and 500) is not sufficient for the effective taste masking. The present finding is rather surprising since the multiple TiO₂ nanolayers were expected to act as effective barriers to prevent water and oxygen penetration, and thus delay the onset of denatonium benzoate release, and moreover, as Lehtonen and co-workers (2013) reported about the delay in the onset of drug release of TiO₂ ALD layered vitamin C tablets as well as the taste and smell masking of ALD coated fish oil soft gelatin capsules. In our study, only negligible delay in the dissolution of denatonium benzoate from TiO₂ coated minitables was observed, this regarding minitables coated with 500 coating cycles. Furthermore, no statistical significant difference ($p>0.05$) was found between the early-stage dissolution (within 45 s – 1 min 15 s) of TiO₂ ALD layered minitables compared to uncoated minitables.

We found that the minitables coated with a polymer amount of 8 mg/cm² are evidently applicable for the bitter taste masking of denatonium benzoate. The present fluidized-bed coated minitables exhibited the most extensive delay in the onset of disintegration and dissolution *in vitro* (Fig. 2 and Table 2). However, it should be emphasized that the dissolution and mechanical properties (softening) of these polymer film coated minitables are greatly dependent on the fluidized-bed coating conditions. The ALD thin coating method has some advantages over fluidized-bed coating conditions. The ALD nanolayering is a simple and rapid method, and

547 especially applicable in case of moisture sensitive tablet formulations since tablet cores are not
548 exposed to high humidity conditions similar to those in fluidized-bed coating. Consequently,
549 ALD nanolayering should not affect the physicochemical and pharmaceutical properties of
550 tablets. Our results suggest also that the adequate taste masking efficacy of minitables could be
551 achieved by increasing the number of coating cycles in the TiO_2 ALD nanolayering, as the
552 release of bitter tasting denatonium benzoate was, though only slightly, delayed from minitables
553 coated with 500 coating cycles. Attention should also be put onto the time required for the
554 precursor pulse, as the unexpected dissolution of TiO_2 coated minitables could be also explained
555 by the pulse of 300 ms being possibly inadequate for precursors to penetrate into the tablet pores.
556 In addition, the coating materials other than TiO_2 or the multilayer ALD coatings could also open
557 new alternatives to single ALD thin coatings for taste masking applications. For example, Al_2O_3
558 ALD thin coated tablets have been shown to exhibit faster drug release in water in comparison to
559 TiO_2 ALD coated tablets (Lehtonen et al., 2013). The use of an ALD coating system (reactor)
560 other than the flow type one could also provide improvements in taste masking efficiency.
561 Carlsson and co-workers (2016) reported the existence of holes in the ALD coated nanoparticles
562 due to the contact points with other nanoparticles during deposition. In theory, this could be also
563 possible with the present TiO_2 ALD thin-coated minitables, since the exposure of stationary
564 tablet(s) to ALD could lead to disruptions in thin coatings due to the direct contact of the tablet
565 lower surface with an ALD tray. The probability for the formation of uncoated contact points in
566 minitables, however, is minimal, since the tablets are slightly vibrating in the semifluid state
567 during the flow of ALD coating. Therefore, the major reason for the defects of TiO_2 ALD thin
568 coating (and obviously for a limited taste masking efficacy of minitables) is the heterogeneous
569 structure of the tablet surface. It is evident that the surface moisture is adequate for ALD and for

the formation of even TiO₂ nanolayers, but the affinity of some tablet excipients varies a lot and this can prevent the formation of homogeneous and continuous TiO₂ nanolayers.

4.3 Surface morphology and content analysis

The surface properties of fluidized-bed film coated minitabets were dependent on the amount of coating polymer used. The minitabets coated with the lowest polymer amount of 2 mg/cm² exhibited a large variation in film coating appearance (quality) due to erosion and tablet breakage (Fig. 3E). The tablets coated with the highest polymer amount of 8 mg/cm² had an intact and smooth surface (Fig. 3H). The actual coating thickness of polymer coated tablets ranged from some tenths of micrometers (2 mg/cm²) to a few hundred micrometers (8 mg/cm²). Such great variation in coating thicknesses (and intactness) explains also the changes in physical and pharmaceutical properties of minitabets coated with different amounts of polymer.

Since SEM did not permit the nanometer-scale analysis of the ALD nanolayered minitabets, the surface of an uncoated and a TiO₂ coated (500 cycles) minitabes was analyzed also with SEM-EDS. This analysis (elemental mapping) was primarily carried out to explain the accelerated disintegration and dissolution behavior of ALD thin-coated minitabets. The presence of Ti signal on the porous ALD coated minitabes surface can be considered as an important verification on the successful nanolayer formation onto the surface of minitabets. In accordance to the theory on hermetic ALD layers on porous minitabets, the SEM-EDS results suggested that the TiO₂ layer was integral and indeed entirely covering the various areas over the linescan on the minitabes surface leaving no disrupted areas in the coating. Moreover, in agreement with our theory of ALD thin coating on porous tablets, the TiO₂ precursors seem to diffuse into the voids and pores of minitabets with the estimated diffusion length of approximately 100-200 μm. This

finding supports the view that the ALD thin coating of minitables can be successfully performed. The major limitation of the presented coated substrates, however, was that they did not permit us to analyze the interface between the minitab core and nanolayer, and thus to determine the actual thickness of titanium coating. Lehtonen and co-workers (2013) used SEM to measure a nanometer scale Al_2O_3 (10 nm) + TiO_2 (10 nm) layer thickness of fish oil containing soft gel gelatin capsules. In our study, however, the analysis of the interface of tablet core and nanolayers, and coating thickness are much more challenging due to the porous structure of tablet surface compared to that of soft gelatin capsule. Nevertheless, this issue could be overcome by the verification of integral titanium layer on minitables combined with the known theoretical nanocoating thickness.

In addition to titanium, traces of chlorine were also present on TiO_2 ALD coated minitab surface. This is obviously due to a porous substrate and low ALD coating temperature of 65°C which is known to leave residuals of incompletely reacted TiCl_4 on surfaces (Ritala et al., 1993). The residuals present could be minimized by increasing the ALD coating temperature up to and even over 200°C (Ritala et al., 1993). Many active pharmaceutical substances and excipients, however, are thermally sensitive, which limits the use of very high handling temperatures during ALD thin coating. Further studies will be needed on the formation and role of precursor residuals (including safety and toxicity) in ALD nanolayers.

The SEM-EDS morphological and elemental analysis revealed that the surface of uncoated minitables is porous and heterogeneous due to the multiple excipients used for formulating the tablet cores. The surface of uncoated minitables (cores) was covered with the grey-white and dark areas (spots), which were still clearly visible in TiO_2 ALD coated tablets. The bright areas revealed a more intense signal for phosphorous and calcium over dark areas. The presence of

phosphorous and calcium refers to the calcium hydrogen phosphate dihydrate used as an excipient in the minitablet composition. Surprisingly, the behavior of phosphorous and calcium seemed to be followed by an increase in the manifestation for titanium. The difference in titanium intensity between white and dark areas was found to be notable and in contrast to other surface elements. The intensity of titanium was clearly the highest in the white surface areas together with phosphorous and calcium.

The present finding is considered as significant. The high intensity of titanium signals indicates that certain pharmaceutical excipients (such as in our study calcium hydrogen phosphate dihydrate) can be coated (nanolayered) with TiO_2 more easily than others. The differences in the intensity of titanium signals can also indicate the uneven formation of nanolayers on the heterogeneous surface of minitablets, thus resulting in the limited moisture protection and changes of the performance of ALD coated minitablets. However, the formation of uneven nanolayers, can be argued since titanium was also detected in the surface pores of the minitablet cores, and may therefore not be seen there at the equal levels found in the calcium and phosphorous rich surfaces. Further studies will be needed on using TiO_2 nanolayers with both active pharmaceutical substances and excipients.

5. CONCLUSIONS

ALD provides a simple and rapid method for the ultrathin coating (nanolayering) of minitablets. It is evident that the level of agitation and collision forces between tablets in ALD are minor compared to polymer coating in a fluidized-bed, not to mention that the method is relatively simple compared to the conventional and challenging polymer film coating process. The ALD thin coating method has both advantages and limitations over traditional film coating methods.

The ALD thin coating is a rapid process since no spraying and drying steps are needed. However, the unexpected changes in the TiO₂ ALD coated minitab⁶³⁷let mechanical properties seen as an accelerated tablet disintegration rate and decreased tablet hardness may challenge its feasibility in the coating of heterogeneous substrates composed of substances with different chemical characteristics and reaction ability, until a thorough understanding on possible phenomena taking place on tablet surface and within used diverse and physicochemically variable excipients during ALD process is established. Therefore, the major challenges of ALD thin coating are related to the sufficient taste masking capacity and interactions of coating/layering material (TiO₂) with the excipients used in the tablet core. More research is needed to clarify the potential of ALD in tablet coating applications. For example, coating materials other than TiO₂, the effects of the number of coating cycles and the length of the precursor pulses on the taste masking are suggested for further study.

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712

713 Captions to illustrations:

714 **Fig. 1.** The theoretical formation of TiO₂ nanolayers via the chemical reaction between water and
715 TiCl₄ in atomic layer deposition (ALD) thin-coating process. In ALD involving metal oxides, a
716 cycle of surface saturation takes place through two reaction steps performed commonly in
717 vacuum at controlled temperature. During step one (the first half cycle) the metal precursor such
718 as TiCl₄ vapor, pulsed to the coating chamber, is allowed to react with the free hydroxyl groups
719 on the substrate surface. The chemical pulse therefore saturates the surface with Ti containing
720 groups through molecular bonds. During step two (the second half cycle) the molecularly bonded
721 structures on the substrate surface react with the oxygen precursor (water vapor) and form the
722 first nanolayer of TiO₂. Between the steps, a purge of inert gas (N₂) is applied to the chamber to
723 remove the possible excess of precursor and reaction by-products. The film thickness is
724 controlled by repeating the number of reaction cycles to reach the desired coating.

725 **Fig. 2.** Dissolution profiles of uncoated minitablets, TiO₂ ALD (100, 300 and 500 cycles) thin-
726 coated and fluidized-bed polymer film coated (2, 4, 6 and 8 mg/cm² of polymer) minitablets
727 (n=4). The dissolution curves describe the cumulative release of denatonium benzoate from
728 minitablets.

729 **Fig. 3.** Scanning electron microscopy (SEM) images on uncoated minitablet (Fig. 3A), TiO₂
730 ALD thin-coated minitablets (100, 300 and 500 cycles; Fig. 3B-D, respectively) and fluidized-
731 bed polymer film coated minitablets (2, 4, 6 and 8 mg/cm²; Fig. 3E-H, respectively).

732 **Fig. 4.** Scanning electron microscopy-energy dispersive spectroscopy (SEM-EDS) image on the
733 intact TiO₂ ALD thin-coated minitablet (500 cycles). Arrows indicate the presence of titanium on
734 the ALD thin-coated minitablet surface followed by signals on calcium and phosphorous.

735 **Fig. 5.** SEM-EDS image on the cross-section of TiO₂ ALD thin-coated minitablet (500 cycles).

736 **Table 1.** Used parameters for minitabulet polymer coating.

Parameter	Value
Nozzle diameter	0.5 mm
Atomizing air pressure	1.1 bar
Inlet air volume	12.5 l/s
Inlet air temperature	40-50°C
Spraying rate	2.2 g/min

737

738 **Table 2.** Results of the tests performed on both uncoated, and for TiO₂ and EPO coated
739 minitables of the study. Statistically significant (p<0.05) difference between uncoated and
740 coated tablet is marked in bold.

Tablet	Uniformity of mass Average \pm SD (mg)	Uniformity of content Average \pm SD (mg)	Disintegration rate Average \pm SD (s)	Tablet breaking force Average \pm SD (N)	Tablet height Average \pm SD (mm)
Batch I Uncoated	23.0 \pm 0.4	8.6 \pm 0.4	48 \pm 3	50 \pm 4	2.42 \pm 0.02
TiO ₂ coated, 100 cycles	22.7 \pm 0.3	8.3 \pm 0.4	23 \pm 2	45 \pm 2	2.41 \pm 0.03
TiO ₂ coated, 300 cycles	22.8 \pm 0.4	8.5 \pm 0.2	20 \pm 6	43 \pm 3	2.40 \pm 0.02
TiO ₂ coated, 500 cycles	22.7 \pm 0.4	8.7 \pm 0.3	19 \pm 5	44 \pm 4	2.39 \pm 0.02
Batch II Uncoated	24.5 \pm 0.5	10.0 \pm 0.8	44 \pm 8	61 \pm 7	2.46 \pm 0.05
EPO coated, 2 mg/cm ²	23.9 \pm 0.5	9.8 \pm 0.9	16 \pm 2	44 \pm 3	2.46 \pm 0.02
EPO coated, 4 mg/cm ²	24.8 \pm 0.6	9.6 \pm 0.6	25 \pm 3	44 \pm 4	2.51 \pm 0.04

Batch III Uncoated	23.3 ± 0.5	10.0 ± 0.6	31 ± 3	51 ± 3	2.40 ± 0.03
EPO coated, 6 mg/cm ²	24.4 ± 0.6	9.3 ± 0.4	29 ± 4	37 ± 2	2.49 ± 0.03
EPO coated, 8 mg/cm ²	25.5 ± 0.6	9.6 ± 0.8	50 ± 3	41 ± 3	2.54 ± 0.02

741